Dorothy Ian Fred Bruhweiler; Catholic J. Jordan, Fraquelli, Helen Forrest Hamilton, Hart, $\overline{}$ Jniversity Alfred B Mai of So America rk chultz; Computer Kochte; Computer Sciences



from the target-star side of the screen in its observing configuration. The underside of the bus and solar arrays are visible in the foreground in front of the screen. Astromasts or bistems are shown connecting and sup-porting the top and bottom of the screen. The artist's rendition above shows the occulter viewed



tion Plan shown views 0 above are of the observing config from three different perspectives ; configuraRover

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Sun Shad

- Sun Shade
 Occulting Screen
 Pedestal/Cassette & I Boom
- Bus

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- Solar Arrays Propulsion Modules 8 Boom

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Character ristic Solar Array and Bus Sizes for SPIDER in var mission class

Mission	Solar Array	Solar Array	Solar Array	Bus
Class	Y-width	+X-wing	-X-wing	
E-class	4 m	4 x 0.8 m	4 x 0.4 m	1.2 x 1.2 x 1.2 m
D-class	4 m	6 x 1.0 m	4 x 0.5 m	1.5 x 1.5 x 4 m
N-class	12 m	5 x 1.0 m	4 x 0.4 m	1.5 x 1.5 x 6-8 m

Functionally, the occulting screen is used for two purposes:

• • • Occulting the Star. • Hiding other space spacecraft structures (e.g. bus, solar array) from the telescope

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MLI screen construction emphasizes:

optimizing imizing science thermal characteristics for N-class infrarec serving science utility by mitigating meteoroid impact dam mission

pre nage

The Sun Shade allows minimal scattering of sunlight toward the it shades the entire side of the screen facing the telescope. telescope since



UMBRAS/SPIDER **Features:**

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- Occulting Screen unfurled from 'window shade' cassette on Screen Pedestal.
 Controlled 1-time unfurling of Screen & Propulsion Boom Deployment
 'Curtain track' to create larger screen from overlapping layers.
 Bistems or coiled Astromasts for shade/screen support.
 Sun Shade shields screen from direct solar exposure during observations.
 Screen/Pedestal articulates for:

 transit to provide symmetry for thrust control.
 observations to hide bus/array/propulsion from telescope.

 Propulsion Module on boom(s) minimizes contamination & interference.
 Xenon propellant tanks stored in bus.
 Solar Electric Propulsion offers significant observation rates.
 Attitude/Translation Control thrusters mounted on Bus & Propulsion Module.
 3-axis stabilization for stationkeeping, maneuvering, & transits. • •

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3-D renderings of an N-class UMBRAS Occulter courtesy of Edward Rowles, Multi Image Productions, tarships.com/Multi-Image/MIP_Home.HTML ulti-

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repres UMBRAS (Umbral Missions Blocking Radiating Astronomical Sources) is a well as a technique. The general design is scalable for small as well as large of the second statement o as a technique. The general design is scalable for small as well as large occulter, sentative set of missions classes and their general mission design characteristics. class of missions ìГS. Below is as a

up to 6 years	~45 m	4-10+ m	N-Class (NGST)
2+ years	10-30 m	1-4 m	D-Class (Discovery)
~1+ years	m 8-5∽	~ 1 m	E-Class (Explorer)
Duration	Size	Aperture	Class
Mission	Screen	Telescope	Mission

aunch H ackaging

SPIDER sily fits within ÷ d bay

At left we see a cross-section for packaging a large N-class occulter into a Titan-IV fairing or Shuttle payload bay. The solar arrays fold flat against the bus. The propulsion booms fold longitudinally, and the cassette housing the occulting screen is pulled in next to the bus. The Sun Shade is also folded to fit within the fairing. The propulsion

At left is a diagram of an N-class occulter bus with the propulsion booms folded to place the modules alongside the spacecraft bus. Folding rigid booms allow the num-ber of flexible propellant line connections to be minimized. Placement of Attitude & Translation Control (ATCS) thrusters on the bus is shown, with nozzle size exagger-ated for clarity.

At left is the same diagram as described above, however the propulsion booms have been deployed. Note that the propul-sion modules have swung into their opera-tional place. The number of required booms depends upon the number of engines and the packing factor within the launch fairing. Here, we assume 24 needed for smaller missions, or for NSTAR engines with longer life carbon-carbon cathodes replacing current molyb-denum ones. Placement of ATCS thrustengines and the packing factor v launch fairing. Here, we assum-required engines. However, few ers on the propulsion shown. module is als er may be

	E- 5-metr <u>Mass/Powe</u>	class e Screen /Dimensions:	D- 10-mei <u>Mass/Powe</u>	class re Screen r/ <u>Dimensions:</u>	N- 45-mer <u>Mass/Powe</u>	-class tre Screen <u>r/Dimensions:</u>
Payload: extensible screen	13 kg		52 kg		360 kg	
screen cassette	20 kg		40 kg		90 kg	
bus-screen boom metrology (beacons) <u>pedestal & masts</u> <u>Payload subtotal:</u>	30 kg 10 kg <u>50 kg</u> <u>123 kg</u>	[50 W]	30 kg 10 kg <u>100 kg</u> <u>252 kg</u>	[50 W]	70 kg 30 kg <u>130 kg</u> <u>710 kg</u>	[50 W] (inc booms)
Bus + Array:						
<i>Structure:</i> array support bus + propulsion boom	12 kg 75 kg		20 kg 100 kg		50 kg 200 kg	
Power Production & Storage: Arrays (GaAs @ 18% BOL) Power Control & Conversion Battery : (450 W-hrs NiH2)	168 kg 175 kg 10 kg	{4.2 kW}	280 kg 300 kg 10 kg	{7kW}	600 kg 680 kg 10 kg	{15 kW}
Propulsion: NSTAR @92mN ($\eta = .85$)	17kg	(1)	102 kg	(2 op. of 6)	408 kg	(6 op. of 24)
Power Conditioning/Control Xe propellant storage tanks Xe pressure & feed system	30 kg ~ 30 kg 50 kg	[~0.3 kW] (1 units) [100 W]	120 kg ~ 130 kg 50 kg	[~0.6 kW] (4 units) [100 W]	300 kg ~1200 kg 50 kg	[~1.5 kW] (10 units) [100 W]
Attitude & position determination & control: ACS (16 UK-10 @25mN) ACS aux (16 N2 @5N + pinholes)	- 40 kg	[100 W]	< 120 kg 40 kg	(4 x 0.7 kW) [100 W]	< 120 kg 40 kg	(4 x 0.7 kW) [100 W]
sun sensors (4 units) star trackers/optical navigation cameras gyros & reaction wheels	4 kg 3 kg 26 kg	[12W] [40 W] (2 unit) [150 W] (4 each)	4 kg 6 kg 42 kg	[12W] [80 W] (4 units) [150 W] (6 each)	4 kg 6 kg 142 kg	[12 W] [80 W] (4 units) [500 W] (6 each)
Communications: Communications (low gain), 2 units	50 kg	[70 W]	50 kg	[70 W]	150 kg	[170 W]
Command, Control & Data I/O:	$50\mathrm{kg}$	[50 W]	50 kg	[50 W]	50 kg	[50 W]
<u>Thermal Control:</u>	<u>10 kg</u>		<u>20 kg</u>		<u>30 kg</u>	
Bus + Array subtotal	853 kg		1527 kg		4223 kg	
Dry mass:	<u>986 kg</u>		<u>1779 kg</u>		<u>4933 kg</u>	
<u>Margin ~ 20% (total dry mass):</u>	<u>197 kg</u>		<u>356 kg</u>	Π	<u>987 kg</u>	
Xenon Propellant	100 kg		440 kg		4000 kg	
Total mass (inc. propellant):	< 1278 kg		< 2700 kg		<u>< 9860 kg</u>	

Abstract:

the ble using various sion, mass estimates, and power requirements, is presented requiring no extension of existing technology allowing extrasolar planet searches. An occulting spacecraft design, emphasizing configuration, control, propulvations are engineering free-flying occ occulting emple solutions. cra ulter ft to be packaged on existing launchers oyed to block starlight and suppress scattered sunlight. A station keeping control method thruster types. Solar electric propulsion enables scientifically useful observation rates an ' used The design is scalable for use with telescopes having 1 to 10 metre apertures. with a space-based telescope can enhance the contrast in the region close to with no on-orbit assembly. Sever 2 star, nd allows d is possial innoor exotic

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Best guess upper limits on the mass and power budgets for 3 different sized UMBRAS Occulter mission clas

occulter might need a shuttle, Titan IV-class vehicle.

SPIDER

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Above is a control block diagram showing a scheme for controlling the relative position of the occulter with respect to the telescope. Imaging of the occulter against the background stars by cameras onboard the telescope allows the occulter to be appropriately positioned. rel-

achieve science goals. NAS. baselined for this mission. X used for the ATCS (Attitude Solar Electric Propulsion n for primary propulsion is sufficient to NASA/Hughes NSTAR engines are n. XIPS or cold-gas thrusters may be tude & Translation Control Sub-

Thruster plume impingement on the screen is avoided. Attitude control thrusters are located on the propulsion module (B) and the spacecraft bus (A) and allow some T-axis translational motion with little impact on the observation. Shown above is the general scheme of coplanar force-couples, with the center of mass in the plane of the couple, enabling attitude and trans-lational control amidst science observations.

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20.93 metre diameter sphe albedo = 1.0 sun-occulter telescope angle = 45 deg
20.93 metre diameter sphe albedo=1.0 sun-occulter telescope angle = 45 deg

jected area as a 45-(log of separation in bright. 5-metre N-c. n in metres). Z

UMBRAS employs a sun shade to shield sunlight. The Shade's razor-like edge is c mize sunlight scattering from the edge in is designed to mini-e into the telesco

edges illuminated by the sun, for two different edge sharp-nesses. Note that the edge is much less bright than the spheres shown above. The specular curves are for an ori-entation with the brightness at a maximum (viewer perpen-dicular to the edge). Properly oriented, the shade reflects most of this away from the telescope. Vapor deposition of a micro-bead-ing material on the edge could strike a balance minimizing over-all light scattered into the telescope. At right diffuse and specular is shown the bright-

Rover, Telescope Exoplanet Coronagraph Occulting Visible 8

CORVET is a validate the e s a proposed demonstration mission that external free-flying occulter technique. could

S hade

-class An 0000

At left is a close-up of the spacecraft along with its reflection off of the occulting screen. Bistem or astromast supports for the screenwithin field of view) are visible both directly and in reflection rising from the cassette-pedestal structure. and-shade (shade not

- • -metre space teleo Unoccluded,o Focal plane c ch (b Solai th cra orbit escope (~1000] , off-axis prima aft) on or L2
- 0 0 0 0 0 lter (<1300 kg) w/
 5- to 8-metre occulting
 1 NSTAR XIPS engine
 Fuel for 1-2 year mission
 50 bright targets, 2 vision
 Jovian search 0.25" - 4

Earth gravitation on stationkeeping. Occulter ale), to minimize the the and telesc sun, telescope, ope effects of must operate far from ng. At right (not , and occulter lie perations diffe rential lie

in a plane. The occul that the telescope is ir by the occulter. The o is hidden from the tele to s culter is positioned such is in the star-shadow cast he occulter spacecraft bus elescope er spacecraft bus by the screen. cast

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gram showing snapshots of an Nconfiguration for movement between targets. At left is a requires clas the configuration at difconceptual diainto a symmetric SPIDER operation occulting s s occulter articulating creen 5 een

occulter-target plane. Phases (A) and (I) represent successive stations on different Target-Telescope Lines-of-Sight (different science targets). The phases in between show snapshots of the occulter at representative moments during the journey between targets. the telescope

Distinct phases of target-to-target transit operations:

Articulate the screen into transit position. Orient occulter toward next Target-Telescope Li Acceleration toward next Target-Telescope Line Mid-course turnover

Line

ne-of-Sight. -of-Sight.

- • D
- Alignment Articulate id-course turnover eccelerate to a halt. lignment of Occulte ire en into culter 00 along Target-Telescope Line observing configuration. of-Sight.

At left, the N-class occulter transits with the sun in the plane of the occulting screen to minimize solar heating of the screen. This helps the screen reach a lower tem-perature, enabling utility at longer wavelengths than if the screen had to dissipate heat absorbed by more direct solar exposure during transits.

The transit configuration allows and below show the observing a two different mission classes. guration allows simpler control of the spacecraft. The diagrams above the observing and transit configurations of UMBRAS' occulter for ssion classes.

Below, the E- and D-class occulters do not need the extra twist placing the sun in the plane of the screen that the N-class do since smaller telescopes are not likely to be efficient planet hunters at wavelengths where thermal emission by the screen would compromise science objectives.

each at $\lambda =$

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